

A Note on the Modeling of Transmission-Line Losses

Antonije R. Djordjević, Alenka G. Zajić, Dejan V. Tošić, and Truc Hoang

Abstract—We consider uniform lossy transmission lines characterized by their primary parameters. Exact and approximate formulas for the characteristic impedance and propagation coefficient are reviewed and discussed for low-loss lines. Approximating the characteristic impedance by its real part can lead to erroneous results for the input impedance of short- and open-circuited stubs. This problem is analytically demonstrated on electrically short stubs. Results obtained using the exact and approximate expressions are compared with numerical solutions that are generated by various circuit simulation software.

Index Terms—Circuit simulation, distributed parameter circuits, lossy circuits, modeling, simulation software, transmission-line theory.

I. INTRODUCTION

IN THIS paper, we consider the classical problem of transmission-line modeling by circuit-theory equations. This modeling is important because it often represents the first cut in the analysis and design of microwave circuits and because it is sufficiently accurate for lower microwave frequencies. Electromagnetic simulation can be used for more accurate design to include fringe fields, parasitics, radiation, etc.

We assume the line to be uniform and in the sinusoidal regime at the angular frequency ω . The line is described by its primary parameters: 1) L' : per-unit-length inductance; 2) C' : per-unit-length capacitance; 3) R' : per-unit-length resistance; and 4) G' : per-unit-length conductance. The line length is D .

From the telegraphers' equations, one can derive the exact expressions for the characteristic impedance of the line

$$Z_c = \sqrt{\frac{R' + j\omega L'}{G' + j\omega C'}} \quad (1)$$

and the propagation coefficient

$$\gamma = \sqrt{(R' + j\omega L')(G' + j\omega C')}. \quad (2)$$

For most microwave transmission lines, conductor and dielectric losses are relatively low. Hence, we may assume

$$R' \ll \omega L' \quad (3)$$

$$G' \ll \omega C'. \quad (4)$$

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A. R. Djordjević, A. G. Zajić, and D. V. Tošić are with the School of Electrical Engineering, University of Belgrade, 11120 Belgrade, Serbia, Yugoslavia.

T. Hoang was with AIMTA Inc., Fremont, CA 94538 USA. He is now with LTCC Operations, Skyworks Solutions Inc., Fremont, CA 94538 USA.

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Based on the above assumptions, the characteristic impedance is often approximated as purely real and given by

$$Z_c \approx \sqrt{\frac{L'}{C'}}. \quad (5)$$

This expression is commonly used in practice.

The propagation coefficient is usually properly taken to be complex, i.e., $\gamma = \alpha + j\beta$, where α is the attenuation coefficient and β is the phase coefficient. After expanding in a series, the propagation coefficient can be approximately evaluated as

$$\gamma \approx \frac{R'}{2\sqrt{\frac{L'}{C'}}} + \frac{G'}{2\sqrt{\frac{C'}{L'}}} + j\omega\sqrt{L'C'} \quad (6)$$

where

$$\alpha = \frac{R'}{2\sqrt{\frac{L'}{C'}}} + \frac{G'}{2\sqrt{\frac{C'}{L'}}} \quad (7)$$

and

$$\beta = \omega\sqrt{L'C'}. \quad (8)$$

The attenuation coefficient can be represented as the sum of two terms $\alpha = \alpha_c + \alpha_d$, where the first term

$$\alpha_c = \frac{R'}{2\sqrt{\frac{L'}{C'}}} \quad (9)$$

is due to the conductor losses, and the second term

$$\alpha_d = \frac{G'}{2\sqrt{\frac{C'}{L'}}} \quad (10)$$

is due to the dielectric losses.

The aim of this paper is to call attention to a problem that can be encountered when previous approximations are used in the analysis of short- and open-circuited transmission-line sections (stubs). The approximation (5) leads to erroneous evaluation of transmission-line losses, which ultimately affect analysis results for the whole microwave network.

In Section II, this problem is analytically demonstrated on electrically short stubs. These results are numerically verified in Section III. In that section, we compare results obtained using the exact and approximate expressions from Sections I and II

with numerical solutions generated by various circuit simulation software [1].^{1 2 3 4 5}

II. SHORT-LENGTH LOSSY STUBS

Let us consider an electrically short section of a uniform lossy transmission line. We shall analyze the input impedance of short- and open-circuited sections using the exact and approximate expressions for the characteristic impedance and propagation coefficient.

A. Short-Circuited Stub

The exact expression for the input impedance of a short-circuited line is

$$Z_{\text{ins}} = Z_c \tanh(\gamma D). \quad (11)$$

For a short line, $|\gamma D| \ll 1$, thus, we can approximate the hyperbolic tangent in (11) by

$$\tanh(\gamma D) \approx \gamma D. \quad (12)$$

Hence, $Z_{\text{ins}} \approx Z_c \gamma D$. Using the exact expressions (1) and (2), we further obtain

$$Z_{\text{ins}} \approx (R' + j\omega L')D \quad (13)$$

where $R'D$ is the total (series) resistance of the line and $L'D$ is the total inductance. The result given by (13) is obvious for a microwave practitioner: the line approximately acts like an inductor whose quality factor is $Q_L = \omega L'/R'$.

If we use (5) and (6) instead of (1) and (2), we obtain in a similar way from (11)

$$\begin{aligned} Z_{\text{ins}} &\approx \sqrt{\frac{L'}{C'}} \left(\alpha_c + \alpha_d + j\omega \sqrt{L'C'} \right) D \\ &= \left(\frac{R'}{2} + \frac{G'L'}{2C'} + j\omega L' \right) D. \end{aligned} \quad (14)$$

In comparison with (13), (14) yields the same result for the imaginary part, but a different expression for the real part of the input impedance. Hence, the quality factors obtained from (13) and (14) are also different. For example, if the conductor losses dominate (i.e., if $\alpha_c \gg \alpha_d$), (14) yields a two times smaller real part than (13), and, hence, a $2 \times$ higher quality factor. If the dielectric losses dominate (i.e., if $\alpha_c \ll \alpha_d$), (14) gives overestimated losses, i.e., an underestimated quality factor. We shall demonstrate in Section III that (13) gives numerical results similar to (11). The different result obtained from (14) is primarily due to using (5) instead of (1).

¹*Microwave Harmonica PC, ver. 6.0*, Compact Software Inc., Paterson, NJ, 1994.

²*SuperStar, professional ver. 6.5B*, Eagleware Corporation, Norcross, GA, 1999.

³*Microwave Office 2001, ver. 4.00*, Applied Wave Research Inc., El Segundo, CA, 2001.

⁴*Touchstone 1.45*, EESof, Westlake Village, CA, 1985.

⁵*PSpice 9.2*, Cadence Design Systems Inc., San Jose, CA, 2000.

B. Open-Circuited Stub

Now, let us consider a dual situation, i.e., an open-circuited transmission line. The exact input admittance to the line is

$$Y_{\text{ino}} = Y_c \tanh(\gamma D) \quad (15)$$

where $Y_c = 1/Z_c$ is the characteristic admittance of the line.

Using (1), (2), and (12), we obtain

$$Y_{\text{ino}} \approx (G' + j\omega C')D \quad (16)$$

where $G'D$ is the total (parallel) conductance of the line and $C'D$ is the total capacitance. This line acts like a capacitor whose quality factor is $Q_C = \omega C'/G'$.

If we use (5) and (6) instead of (1) and (2), we obtain

$$\begin{aligned} Y_{\text{ino}} &\approx \sqrt{\frac{C'}{L'}} \left(\alpha_c + \alpha_d + j\omega \sqrt{L'C'} \right) D \\ &= \left(\frac{R'C'}{2L'} + \frac{G'}{2} + j\omega C' \right) D. \end{aligned} \quad (17)$$

In comparison with (16), (17) yields the same imaginary part, but a different real part of the input admittance. If the conductor losses on the transmission line dominate (i.e., if $\alpha_c \gg \alpha_d$), (17) gives overestimated losses. If the dielectric losses dominate (i.e., if $\alpha_c \ll \alpha_d$), (17) yields a $2 \times$ better quality factor than (16).

III. NUMERICAL EXAMPLE

To investigate and illustrate the sources of discrepancy among various formulas of Section II, we consider a numerical example. It is a transmission line with the following primary parameters, which are realistic data for a microstrip line at 1 GHz [2].

- $L' = 228.8 \text{ nH/m}$.
- $C' = 91.54 \text{ pF/m}$.
- $R' = 7.640 \Omega/\text{m}$.
- $G' = 485.2 \mu\text{S/m}$.

The line is assumed to be short circuited and its length is assumed to be $D = 10 \text{ mm}$.

As summarized in Table I (Case #1), the characteristic impedance of the line, according to (1), is $Z_c = (49.99 - j0.1118) \Omega$. The propagation coefficient, according to (2), is $\gamma = (0.088537 + j28.755) \text{ m}^{-1}$. From γ , one can calculate the attenuation coefficient $\alpha = 0.7690 \text{ dB/m}$ (most of which is due to the conductor losses because $\alpha_c = 0.6636 \text{ dB/m}$) and evaluate the effective relative permittivity $\epsilon_{re} = 1.882$. Hence, the line length (D) is much shorter than the wavelength ($\lambda = 218 \text{ mm}$).

Three approximations are introduced in Sections I and II, given by (5), (6), and (12), respectively. Each one can be used alone or in a combination with other approximations. To estimate the influence on the input impedance of the line, we introduce one approximation at a time. The results are given as Cases #2–#4 in Table I.

The approximation of the propagation coefficient [see (6)] has a negligible influence.

TABLE I
INPUT IMPEDANCE OF A SHORT-CIRCUITED TRANSMISSION LINE

Case	Formulas used	Z_c [Ω]	γ [m ⁻¹]	Z_{ins} [Ω]
#1	Exact Z_c , γ , tanh (1), (2), (11)	49.99476 – j0.11176	0.0885368 + j28.7551	0.081187 + j14.78569
#2	Exact Z_c , γ Approximate tanh (13)	49.99476 – j0.11176	0.0885368 + j28.7551	0.076400 + j14.37593
#3	Exact Z_c , tanh Approximate γ (1), (6), (11)	49.99476 – j0.11176	0.0885370 + j28.7550	0.081188 + j14.78566
#4	Exact γ , tanh Approximate Z_c (5), (2), (11)	49.9945	0.0885368 + j28.7551	0.048135 + j14.78574
#5	Approximate Z_c , γ , tanh (14)	49.994537	0.0885370 + j28.7550	0.044264 + j14.37593
#6	Touchstone model			0.093660 + j14.78565

The approximation of the hyperbolic tangent [see (13)] introduces an error of approximately -6% for the real part of the input impedance and -3% for the imaginary part. This error diminishes for shorter line lengths.

The approximation of the characteristic impedance [see (5)] is critical. The resulting characteristic impedance is real and practically identical to the real part of (1). The difference is only in the small imaginary part, whose magnitude is approximately 0.2% of the real part. Although small, this number has the major impact on the real part of the input impedance. The resulting error is -41% , as predicted in Section II. In contrast, the approximation (5) has practically no influence on the imaginary part of the input impedance.

The combination of all three approximations, given by (14), gives practically the same imaginary part as (13). The real part given by (14) is significantly smaller, which, again, is attributed to using (5) instead of (1).

All microwave circuit simulators and many “low-frequency” simulators implement a transmission line as the circuit element. Usually there are two models of the line. One is a lossless line, defined by its characteristic impedance and electrical length. The other model, referred to as the physical model, is usually given by the characteristic impedance that is assumed to be real, the attenuation coefficient, and the electrical length. We are interested here only in lossy lines. According to the results shown in Table I, the data that define the physical model are insufficient to produce accurate results for the real part of the input impedance. This insufficiency has been often overlooked by microwave researchers, practitioners, and software developers.

We have evaluated several available software packages, i.e., *Microwave Harmonica PC V6.0*, *SuperStar, professional version 6.5B*, *Microwave Office 2001, version 4.00*, which give identical results for the physical model of the transmission line as in Case #4 of Table I, i.e., they underestimate the real part of the input impedance.

The program *Touchstone 1.45* has a model that tries to bypass the problem of the real characteristic impedance. The model assumes all losses to be due to the conductor losses, i.e., it takes $G' = 0$. It evaluates R' from the given attenuation coefficient and internally computes the characteristic impedance as a complex number. The resulting real part of the input impedance is

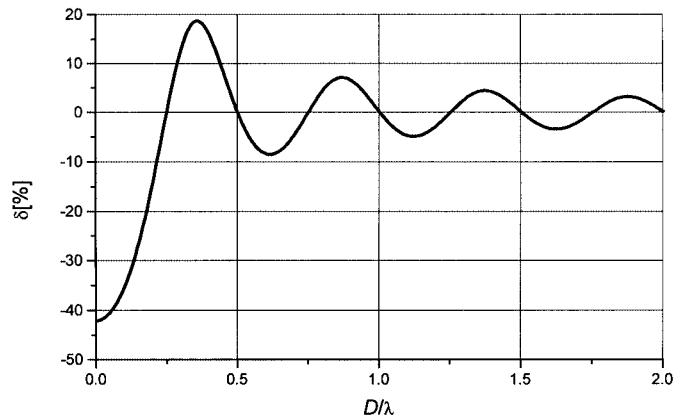


Fig. 1. Relative error in the real part of the input impedance (δ) introduced by using (5) instead of (1) in (11) as a function of the normalized line length (D/λ).

larger than the exact one, as in Case #6 of Table I. The result would be correct only when the dielectric losses are negligibly small.

In certain programs, the input data for defining a lossy transmission line are all four primary parameters and line length. This data set completely describes the line. One example is the program of [1], which uses an exact formulation for the characteristic impedance and gives the same result as in Case #1 of Table I.

In the program *PSpice 9.2*, the standard lossy transmission-line model T-RLGC uses all four primary parameters. However, the result is the same as in Case #4 of Table I. On the other hand, the analog behavior model (ABM) module in this program, from the Library of Transmission Line Models and Subcircuits (tline.lib), gives correct results, as in Case #1 of Table I.

The same problem as investigated for the physical model of the transmission line was also discovered in other models in some programs (e.g., the coupled microstrip lines in *Touchstone 1.45*), but we shall not elaborate on this further.

Fig. 1 presents the relative error in the real part of the input impedance introduced by using (5) instead of (1) in (11), as a function of the line length. The error in the imaginary part is negligibly small, except in the immediate vicinity of resonant lengths. The error in the real part has a maximum for electrically short lines and it vanishes at resonant lengths. The envelope of this error diminishes with an increase in the line length. A more detailed mathematical analysis of this error is beyond the scope of this paper.

For the same transmission line as above, the input admittance is calculated for an open-circuited stub. Equations (1), (2), and (15) give the exact input admittance $Y_{\text{ino}} = (6.0343 + j5915.6) \mu\text{S}$. Equations (16) and (17) give the input admittances $Y_{\text{ino}} = (4.8520 + j5751.6) \mu\text{S}$, and $Y_{\text{ino}} = (17.7093 + j5751.6) \mu\text{S}$, respectively. Equations (2), (5), and (15) yield $Y_{\text{ino}} = (19.2580 + j5915.6) \mu\text{S}$. The last result, with a highly overestimated real part, is also obtained by these programs. *Touchstone* yields $Y_{\text{ino}} = (1.0441 + j5915.6) \mu\text{S}$. The real part is highly underestimated because the loss is

associated only with conductors, whereas the major losses for this short line come from the dielectric (whose quality factor is $Q_C = 1185$).

IV. CONCLUSION

We have considered uniform lossy transmission lines characterized by the primary (per-unit-length) parameters at a given frequency. The lines are assumed to operate in the sinusoidal regime. We have presented exact and approximate formulas for the characteristic impedance and propagation coefficient of low-loss lines. The usual approximation of the complex characteristic impedance by its real part introduces a significant error in the real part of the input impedance of transmission-line stubs. Consequently, the quality factor of the stubs can be overestimated or underestimated. This error is particularly pronounced for electrically short lines. A similar problem occurs in the time-domain analysis of lossy transmission lines of arbitrary lengths. The remedy is to adequately take into account all four primary parameters of the line.

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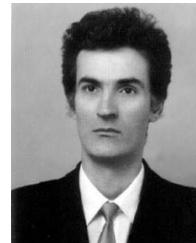


Antonije R. Djordjević was born in Belgrade, Yugoslavia, on April 28, 1952. He received the B.Sc., M.Sc., and D.Sc. degrees from the School of Electrical Engineering, University of Belgrade, Yugoslavia, in 1975, 1977, and 1979, respectively. In 1975, he joined the School of Electrical Engineering, University of Belgrade, as a Teaching Assistant. He was promoted to an Assistant Professor, Associate Professor, and Professor, in 1982, 1988, and 1992, respectively. In 1983, he was a Visiting Associate Professor at the Rochester Institute of Technology, Rochester, NY. Since 1992, he has also been an Adjunct Associate Professor with Syracuse University, Syracuse, NY. His main area of interest is numerical electromagnetics, in particular, as applied to multiconductor transmission lines, wire and surface antennas, and electromagnetic-compatibility problems.



Alenka G. Zajić was born in Belgrade, Yugoslavia, in 1977. She received the B.Sc. degree from the University of Belgrade, Belgrade, Serbia, Yugoslavia, in 2001, and is currently working toward the M.Sc. degree at the University of Belgrade.

She is currently a Design Engineer with Skyworks Solutions Inc., Fremont, CA. Her research interests include solving numerical problems in electromagnetics applied to antennas and passive microwave components, as well as design of RF and passive microwave components.



Dejan V. Tošić was born in Belgrade, Yugoslavia. He received the B.Sc. (1980), M.Sc. (1987), and Ph.D. (1996) degrees in electrical engineering from the School of Electrical Engineering, University of Belgrade, Belgrade, Yugoslavia, in 1980, 1987, and 1996, respectively.

He is currently an Assistant Professor with the School of Electrical Engineering, University of Belgrade. He coauthored *Filter Design for Signal Processing Using MATLAB and Mathematica* (Englewood Cliffs, NJ: Prentice-Hall, 2001). His research interests include signal processing, symbolic analysis and design of circuits, systems, and microwave circuits.



Truc Hoang was born in Saigon, Vietnam, in 1961. He received the B.S. degree in electrical engineering and computer sciences from the University of California at Berkeley, in 1983, and the M.S. degree in electrical engineering from Santa Clara University, Santa Clara, CA, in 1988.

From 1983 to 1985, he was an RF Design Engineer with General Dynamics. Since 1985, he has been with GTE Government Systems, Motorola, CTS, and AIMTA. He is currently with LTCC Operations, Skyworks Solutions Inc., Fremont, CA. His current area of interest is in the continuous improvement of the design flow of low-cost high-yield high-volume RF modules through computer-aided and numerical electromagnetic techniques and tools.